

## **modelization of the vehicle running behaviour on a track (and Excel sheet notice)**

### **principles**

The propulsion force  $F_p$  generated at the vehicle motored wheel is used to overcome the mechanical rolling friction on the wheels, the air friction on the body, the gravity force and the inertia forces (linear inertia and rotational inertia) :

$$F_p \cdot ign = a \cdot m \cdot g \cdot \cos \theta + a' \cdot m \cdot \frac{v^2}{R} + \frac{1}{2} \rho \cdot S \cdot C_x \cdot v^2 + m \cdot g \cdot \sin \theta + (m + m_i) \frac{dv}{dt} \quad (1)$$

hence 
$$\frac{dv}{dt} = \frac{[F_p \cdot ign - m \cdot g \cdot (a \cdot \cos \theta + \sin \theta)] - (\frac{a' \cdot m}{R} + \frac{1}{2} \rho \cdot S \cdot C_x) \cdot v^2}{(m + m_i)} = A - Bv^2 \quad (2)$$

$$dx = v \cdot dt = \frac{v \cdot dv}{A - B \cdot v^2} = \frac{dv^2}{2(A - B \cdot v^2)} = \frac{du}{2B(\frac{A}{B} - u)} \quad (3)$$

where (approximate values for prototypes are given between parenthesis):

- $a$  axial *mechanical friction constant* referred to the weight of the vehicle (0.002 to 0.005).
- $m$  vehicle mass with pilot (80 to 110kg)
- $a'$  lateral mechanical friction constant (in a curve) referred to the weight of the vehicle (neglected here).
- $m_i$  equivalent mass for the rotational masses
- $\rho$  density of air (app. 1.2kg/m<sup>3</sup>, depending on the weather and altitude)
- $S$  frontal area (0.3 to 0.5m<sup>2</sup>)
- $C_x$  aerodynamic drag coefficient (0.08 to 0.16)
- $v$  instantaneous vehicle speed (for the calculus of the aerodynamic force it would be useful to add to this speed the algebraic value of the axial projection of the wind speed )
- $\theta$  angle of the actual road relative to a horizontal reference
- $R$  wheel radius (0.24 to 0.25m)
- $R$  curve radius (m)
- $T_m$  engine/motor torque ( $T_m \approx 0.3$  to 10Nm, electric motor to gas/Diesel engine)
- $F_p = \frac{T_m \cdot \eta_t}{r \cdot R} F_p$  propulsive force (function of the engine/motor speed  $N_m$  and of the throttle opening  $\alpha_{gaz}$ )
- $ign$  switch-on symbol (value : 0 if engine is off, 1 if engine is on)
- $\eta_t$  transmission efficiency (from 0.9 to 0.98)
- $r$  gear ratio (= number of pinion teeth/number of crown teeth, 0.1 as an order of magnitude for one-stage transmission)

**Remark:** during free-wheeling (coasting) on a steep downhill road, A is usually positive for  $-(a \cdot \cos \theta + \sin \theta) > 0$

One considers road sections (between abscissas  $x_i$  and  $x_{i+1}$  with an initial speed  $v_i$  at time  $t_i$ ) for which A and B have quasi-constant values ; the solving of equations (2) and (3) under definite integral forms, gives,

$$* \text{ if } A < 0 : t_{i+1} - t_i = \frac{-1}{\sqrt{|A|B}} \left[ \tan^{-1} \left( \sqrt{\frac{B}{|A|}} v_{i+1} \right) - \tan^{-1} \left( \sqrt{\frac{B}{|A|}} v_i \right) \right] \quad (2')$$

$$x_{i+1} - x_i = \Delta x_i = \frac{-1}{2B} \left[ \log \left( \frac{|A|}{B} + v_{i+1}^2 \right) - \log \left( \frac{|A|}{B} + v_i^2 \right) \right] = \frac{-1}{2B} \left[ \log \left| 1 - \frac{B}{A} v_{i+1}^2 \right| - \log \left| 1 - \frac{B}{A} v_i^2 \right| \right] \quad (3')$$

Remark : letting  $\sqrt{\frac{|A|}{B}} = v_0^-$  (constant), equations (2') and (3') become

$$t_{i+1} - t_i = \frac{-1}{B \cdot v_0^-} \left[ \tan^{-1}\left(\frac{v_{i+1}}{v_0^-}\right) - \tan^{-1}\left(\frac{v_i}{v_0^-}\right) \right] \quad (2'')$$

$$x_{i+1} - x_i = \Delta x_i = \frac{-1}{2B} \left[ \log \left| 1 + \left(\frac{v_{i+1}}{v_0^-}\right)^2 \right| - \log \left| 1 + \left(\frac{v_i}{v_0^-}\right)^2 \right| \right] \quad (3'')$$

knowing  $\Delta x_i$  and  $v_i$ , one deduces  $v_{i+1}$  from (3'') then, knowing  $t_i$  one deduces  $t_{i+1}$  from (2'')

$$\text{* if } A > 0 : t_{i+1} - t_i = \frac{1}{2\sqrt{AB}} \left[ \log \left| \frac{\sqrt{\frac{A}{B}} + v_{i+1}}{\sqrt{\frac{A}{B}} - v_{i+1}} \right| - \log \left| \frac{\sqrt{\frac{A}{B}} + v_i}{\sqrt{\frac{A}{B}} - v_i} \right| \right] = \frac{1}{2\sqrt{AB}} \left[ \log \left| \frac{1 + \sqrt{\frac{B}{A}} v_{i+1}}{1 - \sqrt{\frac{B}{A}} v_{i+1}} \right| - \log \left| \frac{1 + \sqrt{\frac{B}{A}} v_i}{1 - \sqrt{\frac{B}{A}} v_i} \right| \right] \quad (2''')$$

$$x_{i+1} - x_i = \Delta x_i = \frac{-1}{2 \cdot B} \left[ \log \left| \frac{A}{B} - v_{i+1}^2 \right| - \log \left| \frac{A}{B} - v_i^2 \right| \right] = \frac{-1}{2B} \left[ \log \left| 1 - \frac{B}{A} v_{i+1}^2 \right| - \log \left| 1 - \frac{B}{A} v_i^2 \right| \right] \quad (3''')$$

Remark : the energy consumption per unit distance  $\Delta E / \Delta x_i$  (engine on  $\rightarrow ign = 1$  and engine off  $\rightarrow ign = 0$ ) is a function of engine speed  $N_m$ , throttle opening  $\alpha_{gaz}$ , gear ratio and wheel radius.

Remark : letting  $\frac{A}{B} = v_0^2$  (constant), equations (2'') et (3'') become :

$$t_{i+1} - t_i = \Delta t = \frac{1}{2 \cdot B \cdot v_0} \left[ \log \left| \frac{1 + \frac{v_{i+1}}{v_0}}{1 - \frac{v_{i+1}}{v_0}} \right| - \log \left| \frac{1 + \frac{v_i}{v_0}}{1 - \frac{v_i}{v_0}} \right| \right] \quad (2''')$$

$$x_{i+1} - x_i = \Delta x = \frac{-1}{2 \cdot B} \left[ \log \left| 1 - \left(\frac{v_{i+1}}{v_0}\right)^2 \right| - \log \left| 1 - \left(\frac{v_i}{v_0}\right)^2 \right| \right] \quad (3''')$$

average speed on the segment  $x_i$  to  $x_{i+1}$  is

$$v_{ave} = \frac{x_{i+1} - x_i}{t_{i+1} - t_i} = -v_0 \cdot \frac{\left[ \log \left| 1 - \left(\frac{v_{i+1}}{v_0}\right)^2 \right| - \log \left| 1 - \left(\frac{v_i}{v_0}\right)^2 \right| \right]}{\left[ \log \left| \frac{1 + \frac{v_{i+1}}{v_0}}{1 - \frac{v_{i+1}}{v_0}} \right| - \log \left| \frac{1 + \frac{v_i}{v_0}}{1 - \frac{v_i}{v_0}} \right| \right]} \quad (4)$$

## **use of the *elementary driving model* Excel sheet**

to simplify the development of the model, we have made some assumptions :

- the car runs on a **straight level road without wind**
- the mechanical friction factor  $a$  is a constant
- the aero dynamical friction force depends on the square of the running speed
- its factor depends only on the frontal area (effect of wet area is included in the aero dynamical friction factor/drag factor)
- the engine/motor torque is constant during motoring
- the gear ratio is fixed during the run (no clutch or tire slide)
- on each line (from line 14), minimum and maximum speeds are imposed with increasing difference : the start speed and end speed of a sequence are the same and equal to minimum speed, after start the engine is cut-off when the maximum speed is reached
- the engine/motor efficiency is constant, as well as the transmission efficiency
- the free wheel friction is included, taking into account its relative operating time, in the mechanical friction factor
- usually, there is a constant energy cost at each engine/motor start

### ***column contents (from line 14) :***

column A : minimum speed (start and end speed)

column B : maximum speed (speed at cut-off)

column C : distance run during the motoring phase

column D : duration of this phase

column E : distance run during the coasting phase

column F : duration of this phase

column G : total distance run during the sequence (motoring phase + coasting phase)

column H : duration of these 2 phases (the sequence)

column I : energy consumed by the engine/motor during motoring phase

column J : specific energy related to the total distance

column K : specific distance run per unit of energy (1kWh)

column L : average speed on the distance

column M : energy consumed (in kJ) for the length of the run

column N : minimum engine/motor speed corresponding to the minimum car speed (useful in the case of a speed limit imposed by a centrifugal clutch, for example)

column O : maximum engine/speed corresponding to the maximum car speed (useful in the case of a speed limit imposed by a mechanical constraint)

column P : specific distance run per liter of unleaded gasoline (or as an equivalent for other sources of energy)

column Q : approximate number of sequences during a lap

column R : motoring time ratio (depends mainly on propulsion force)